

**Amendments to the Claims:**

The following listing of claims will replace all prior versions, and listings, of claims in the application:

1.-18. (Canceled)

19. (New) An optical integrator, comprising:

an integrally formed plurality of first minute refraction surfaces; and  
an integrally formed plurality of second minute refraction surfaces, which are provided closer to a light emission side than the plurality of first minute refraction surfaces so that the plurality of second minute refraction surfaces optically correspond to the plurality of first minute refraction surfaces, wherein

a parameter  $\beta$  satisfies the following conditions:

$$|\beta| < 0.2 \text{ (where } \beta = (\gamma - 1)^3 \cdot NA^2 / \Delta n^2 \text{), where}$$

a refracting power ratio  $\varphi_a / \varphi_b$  between  $\varphi_a$ , a refracting power of the first minute refraction surfaces and  $\varphi_b$ , a refracting power of the second minute refraction surfaces is  $\gamma$ , numerical aperture on the emission side of the optical integrator is  $NA$ , and a difference between a refraction index of a medium on a light entrance side of the second minute refraction surfaces and a refraction index of a medium on a light emission side of the second minute refraction surfaces is  $\Delta n$ .

20. (New) The optical integrator according to claim 19,

wherein the plurality of first minute refraction surfaces and the plurality of second minute refraction surfaces are formed on the same optical member.

21. (New) The optical integrator according to claim 20,

wherein the plurality of second minute refraction surfaces comprise aspherical surfaces.

22. (New) The optical integrator according to claim 19, comprising:
  - a first optical member having the plurality of first minute refraction surfaces; and
  - a second optical member having the plurality of second minute refraction surfaces arranged on a light emission side of the first optical member.
23. (New) The optical integrator according to claim 22, wherein the plurality of second minute refraction surfaces comprise aspherical surfaces.
24. (New) The optical integrator according to claim 19, wherein each minute refraction surface is formed spherically or aspherically.
25. (New) The optical integrator according to claim 24, wherein the aspherical surface is a rotational symmetry aspherical surface or a rotational asymmetry aspherical surface.
26. (New) The optical integrator according to claim 19, which is used for an exposure apparatus, wherein a mask and a photosensitive substrate are relatively moved in relation to the projection optical system along a scanning direction, and thereby a pattern of the mask is projected and exposed on the photosensitive substrate, wherein an absolute value of the parameter  $\beta$  in terms of a direction optically approximately perpendicular to the scanning direction is set lower than an absolute value of the parameter  $\beta$  in terms of the scanning direction.
27. (New) An illumination optical device for illuminating an irradiated surface, comprising:
  - the optical integrator according to claim 19.
28. (New) The illumination optical device according to claim 27, wherein the

optical integrator forms a light intensity distribution in a given shape in an illumination region.

29. (New) An exposure apparatus, comprising:  
the illumination optical device according to claim 27; and  
a projection optical system for projecting and exposing a pattern of a mask arranged on the irradiated surface on a photosensitive substrate.

30. (New) The exposure apparatus according to claim 29, wherein  
the pattern of the mask is projected and exposed on the photosensitive substrate by relatively moving the mask and the photosensitive substrate in relation to the projection optical system along a scanning direction, and wherein  
an absolute value of the parameter  $\beta$  in terms of a direction optically approximately perpendicular to the scanning direction is set lower than an absolute value of the parameter  $\beta$  in terms of the scanning direction.

31. (New) An exposure method, comprising the steps of:  
illuminating a mask through the illumination optical device according to claim 27, and  
projecting and exposing an image of a pattern formed on the illuminated mask on a photosensitive substrate.

32. (New) The exposure method according to claim 31, wherein  
the step of projecting and exposing an image of a pattern formed on the illuminated mask on a photosensitive substrate comprises the step of projecting and exposing the pattern of the mask on the photosensitive substrate while relatively moving the mask and the photosensitive substrate in relation to the projection optical system along a scanning direction, and wherein  
an absolute value of the parameter  $\beta$  in terms of a direction optically

approximately perpendicular to the scanning direction is set lower than an absolute value of the parameter  $\beta$  in terms of the scanning direction.

33. (New) An optical integrator, comprising in the order from a light entrance side:

a first optical member having an integrally formed plurality of first minute refraction surfaces; and

a second optical member having an integrally formed plurality of second minute refraction surfaces, which are provided to optically correspond to the plurality of first minute refraction surfaces, wherein

a refraction index of an optical material forming the second optical member is set larger than a refraction index of an optical material forming the first optical member.

34. (New) The optical integrator according to claim 33, satisfying the following condition:

$0.05 \leq nb-na$ , where

the refraction index of the optical material forming the first optical member is  $na$ , and the refraction index of the optical material forming the second optical member is  $nb$ .

35. (New) The optical integrator according to claim 34, which is used for light having a wavelength of 300 nm or less, wherein

the optical material forming the first optical member includes silica glass or fluorite, and wherein

the optical material forming the second optical member includes one material of magnesium oxide, ruby, sapphire, quartz crystal, and silica glass.

36. (New) The optical integrator according to claim 33, which is used for light having a wavelength of 300 nm or less, wherein

the optical material forming the first optical member includes fluorite, and  
wherein

the optical material forming the second optical member includes silica glass.

37. (New) The optical integrator according to claim 33, wherein

each minute refraction surface is formed spherically or aspherically.

38. (New) The optical integrator according to claim 24, wherein

the aspherical surface is a rotational symmetry aspherical surface or a  
rotational asymmetry aspherical surface.

39. (New) The optical integrator according to claim 33, which is used for an  
exposure apparatus, wherein a mask and a photosensitive substrate are relatively moved in  
relation to the projection optical system along a scanning direction, and thereby a pattern  
of the mask is projected and exposed on the photosensitive substrate, wherein

an absolute value of the parameter  $\beta$  in terms of a direction optically  
approximately perpendicular to the scanning direction is set lower than an absolute value of  
the parameter  $\beta$  in terms of the scanning direction.

40. (New) An illumination optical device for illuminating irradiated surface,  
comprising:

the optical integrator according to claim 33.

41. (New) The illumination optical device according to claim 40, wherein the  
optical integrator forms a light intensity distribution in a given shape in an illumination  
region.

42. (New) An exposure apparatus, comprising:

the illumination optical device according to claim 40; and

a projection optical system for projecting and exposing a pattern of a mask  
arranged on the irradiated surface on a photosensitive substrate.

43. (New) The exposure apparatus according to claim 42, wherein  
the pattern of the mask is projected and exposed on the photosensitive  
substrate by relatively moving the mask and the photosensitive substrate in relation to the  
projection optical system along a scanning direction, and wherein  
an absolute value of the parameter  $\beta$  in terms of a direction optically  
approximately perpendicular to the scanning direction is set lower than an absolute value of  
the parameter  $\beta$  in terms of the scanning direction.

44. (New) An exposure method, comprising the steps of:  
illuminating a mask through the illumination optical device according to  
claim 40, and  
projecting and exposing an image of a pattern formed on the illuminated  
mask on a photosensitive substrate.

45. (New) The exposure method according to claim 44, wherein  
the step of projecting and exposing an image of a pattern formed on the  
illuminated mask on a photosensitive substrate comprises the step of projecting and  
exposing the pattern of the mask on the photosensitive substrate while relatively moving the  
mask and the photosensitive substrate in relation to the projection optical system along a  
scanning direction, and wherein  
an absolute value of the parameter  $\beta$  in terms of a direction optically  
approximately perpendicular to the scanning direction is set lower than an absolute value of  
the parameter  $\beta$  in terms of the scanning direction.

46. (New) An exposure apparatus, comprising:  
an illumination optical system including an optical integrator; and  
a projection optical system for forming a pattern image of a mask on a  
photosensitive substrate, wherein

the pattern of the mask is projected and exposed on the photosensitive substrate while the mask and the photosensitive substrate are relatively moved in relation to the projection optical system along a scanning direction, wherein

the optical integrator comprises: an integrally formed plurality of first minute refraction surfaces; and an integrally formed plurality of second minute refraction surfaces, which are provided closer to a light emission side than the plurality of first minute refraction surfaces so that the plurality of second minute refraction surfaces optically correspond to the plurality of first minute refraction surfaces, and wherein

a parameter  $\beta$  satisfies the following conditions:

$$|\beta| < 0.2 \text{ (where } \beta = (\gamma - 1)^3 \cdot NA^2 / \Delta n^2 \text{), where}$$

a refracting power ratio  $\varphi_a / \varphi_b$  between  $\varphi_a$ , a refracting power of the first minute refraction surfaces in terms of a nonscanning direction optically approximately perpendicular to the scanning direction and  $\varphi_b$ , a refracting power of the second minute refraction surfaces in terms of the nonscanning direction is  $\gamma$ , numerical aperture on the emission side in terms of the nonscanning direction of the optical integrator is  $NA$ , and a difference between a refraction index of a medium on a light entrance side of the second minute refraction surfaces and a refraction index of a medium on a light emission side of the second minute refraction surfaces is  $\Delta n$ .

47. (New) An exposure method, comprising the steps of:

illuminating a mask through the illumination optical device including an optical integrator, and

projecting and exposing an image of a pattern formed on the illuminated mask on a photosensitive substrate, wherein

the step of projecting and exposing an image of a pattern formed on the illuminated mask on a photosensitive substrate comprises the step of projecting and exposing

the pattern of the mask on the photosensitive substrate while relatively moving the mask and the photosensitive substrate in relation to the projection optical system along a scanning direction, wherein

the optical integrator comprises: an integrally formed plurality of first minute refraction surfaces; and an integrally formed plurality of second minute refraction surfaces, which are provided closer to a light emission side than the plurality of first minute refraction surfaces so that the plurality of second minute refraction surfaces optically correspond to the plurality of first minute refraction surfaces, and wherein

a parameter  $\beta$  satisfies the following conditions:

$$|\beta| < 0.2 \text{ (where } \beta = (\gamma - 1)^3 \cdot NA^2 / \Delta n^2 \text{), where}$$

a refracting power ratio  $\varphi_a / \varphi_b$  between  $\varphi_a$ , a refracting power of the first minute refraction surfaces in terms of a nonscanning direction optically approximately perpendicular to the scanning direction and  $\varphi_b$ , a refracting power of the second minute refraction surfaces in terms of the nonscanning direction is  $\gamma$ , numerical aperture on the emission side in terms of the nonscanning direction of the optical integrator is  $NA$ , and a difference between a refraction index of a medium on a light entrance side of the second minute refraction surfaces and a refraction index of a medium on a light emission side of the second minute refraction surfaces is  $\Delta n$ .